

Result of Analysis of Power System Oscillation Damping & Voltage Stability Improvement Using SSSC in A Multi-Machine System

¹Amit Kumar, ²Pardeep Nain

¹M.Tech Scholar, ²Assistant Professor

EE Department, Om Institute of Technology & Management, Hisar, Haryana, India

ABSTRACT

Interconnection of electric power systems is becoming increasingly widespread as part of the power exchange between countries as well as regions within countries in many parts of the world. There are numerous examples of interconnection of remotely separated regions within one country. In cases of long distance AC transmission, as in interconnected power systems, care has to be taken for safeguarding of synchronism as well as stable system voltages, particularly in conjunction with system faults. With series compensation, bulk AC power transmission over very long distances (over 1000 km) is a reality today. As a result, many power network operators are taking steps to add supplementary damping devices in their systems to improve the system security by damping these undesirable oscillations. With the advent of voltage sourced converter-based series compensation, AC power system interconnections can be brought to their fullest benefit by optimizing their power transmission capability, safeguarding system stability under various operating conditions and optimizing the load sharing between parallel circuits at all times.

Keywords : Static Synchronous Series Compensator (SSSC), Voltage Stability, Power Oscillations Damping (POD), FACTS.

I. INTRODUCTION

Although electricity is a highly engineered product, it is increasingly being considered and handled as a commodity. Thus, the focus on the quality of power delivered is also greater than ever. Series capacitive compensation of power transmission lines is an important and the most economical way to improve power transfer capability, especially when large amounts of power must be transmitted through long transmission lines. However, one of the impeding factors for the increased utilization of series capacitive compensation is the potential risk of Subsynchronous Resonance (SSR), where electrical energy is exchanged with turbine-generator shaft systems in a growing manner which can result in shaft damage. A typical time response of a turbine-generator shaft torsional torque during and after clearing a fault on a series capacitive compensated transmission line in the presence of the SSR phenomenon. It is worth noting here that this shaft is designed to withstand a maximum torsional torque of 2 per unit. Another limitation of series capacitive compensation is its inability to provide adequate damping to power system oscillations after clearing system faults

II. STATIC SYNCHRONOUS SERIES COMPENSATOR (SSSC)

The SVS-based series compensator, called Static Synchronous Series Compensator (SSSC) was proposed by Gyugyi in 1989 within the concept of using converter-based technology uniformly for shunt and series compensation as well as for transmission angle control.

2.1 Phase Control Technique for SSSC

The output of the PI controller is the angle α , which is added to the synchronizing signal Θ passed to the gate pulse generator by the current synchronization block. To this signal $\Theta + \alpha$, an angle of $-\pi/2$ or $+\pi/2$ has to be added since the SSSC output voltage is lagging or leading the line current by 90 depending on the desired capacitive or inductive operation. The phase shift of the converter output voltage V_{SSC} with the respect to the line current I_{line} will cause the flow of a small amount of real power from or into the converter, thereby causing a

change in the dc capacitor voltage, and consequently causing a change in the converter output voltage magnitude .

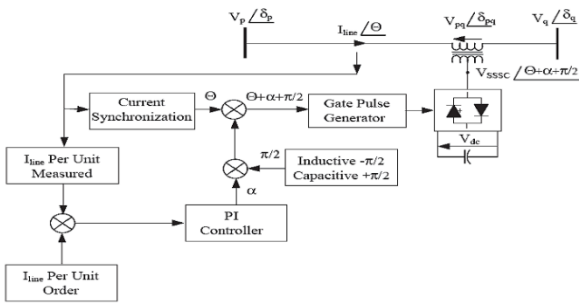


Fig 2.1. Functional control diagram for the phase-controlled SSSC

2.2 PWM Technique

SSSC is modeled as a three-phase, PWM-controlled two-level VSC. The SSSC is modeled in detail, based on an ideal representation of the converter valves and diodes. RC parallel snubber circuits are used to reduce numerical oscillations due to switching, while a series inductance is employed at the converter output to smooth the output current. The series transformer is modeled as an ideal, three-phase, two-winding, Y-Δ connected transformer.

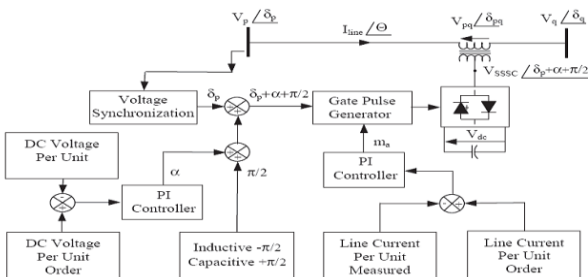


Fig 2.2. Functional control diagram for the PWM-controlled SSSC

2.3 Structure of SSSC-based Damping Controller

1. One of the structures used in this thesis to modulate the SSSC injected voltage is the lead-lag structure as shown in fig.5.11. This structure consists of a gain block, washout block and two stage lead-lag block. The two stage lead-lag block provides the appropriate phase-lead characteristics to compensate for the phase lag between input and the output signals. The washout block acts as a high pass filter to allow signals associated with oscillations to pass as it is. The inputs to the POD controller are the bus voltage at Bus no.2 and the current flowing in Line 1. The Power Oscillation Damping Controller takes input as V_{abc} , I_{abc} & it convert it as power.

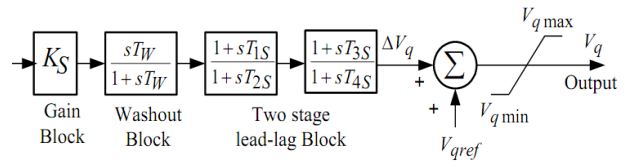


Figure 2.3. POD controller design structure

III. SIMULINK MODELS

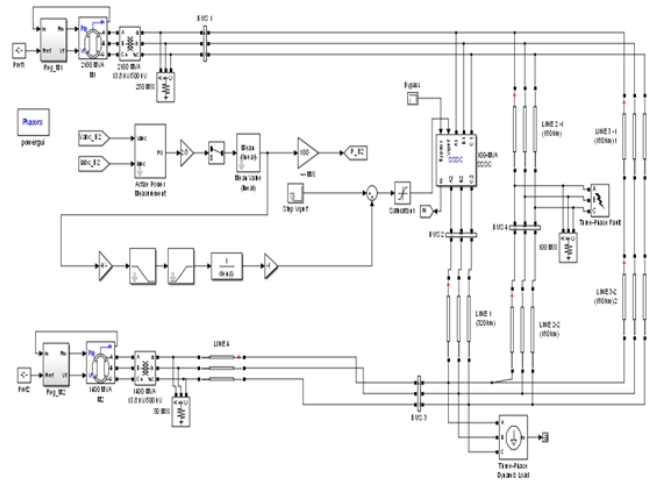


Fig -3.1 Complete Simulation model of test system

3.1 Sub System model:-

3.1.1. POD Model –

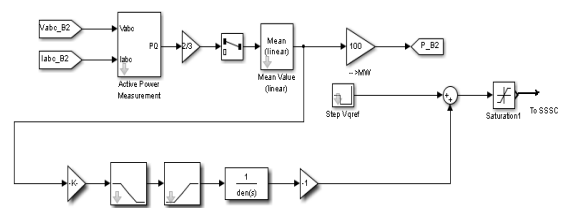


Figure 3.2. Simulink Model of POD controller

3.2 SYMMETRICAL FAULT ANALYSIS

3.2.1. CASE 1: Power flow under normal condition (when POD is OFF, SSSC is by passed and no fault is applied):-

In this case results are calculated under normal condition. Under normal condition SSSC is bypassed using bypass block as shown in simulink diagram, no fault exists, and POD is kept on ‘OFF’ position. Fig 3.3 shows the active power measured at bus no. 2. Fig 3.4 shows the positive sequence components of all bus voltages. Active power and Reactive power measured at all buses are given in fig. 3.5 and 3.6 respectively.

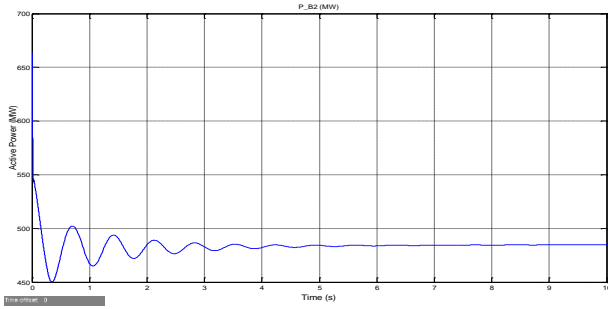


Fig. 3.3. X-axis Show time in sec. and Y-axis Show Active Power in Kw at bus no. 2 During Normal condition (No fault). The Transient Die out in Settling Time (4T).

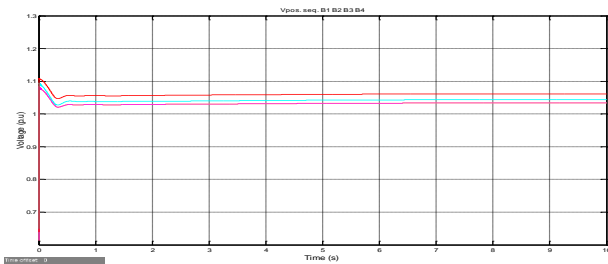


Fig. 3.4. X-axis Show time in sec. and Y-axis Show Positive Sequence voltage at all buses During Normal condition (No fault). The Transient Die out soon.

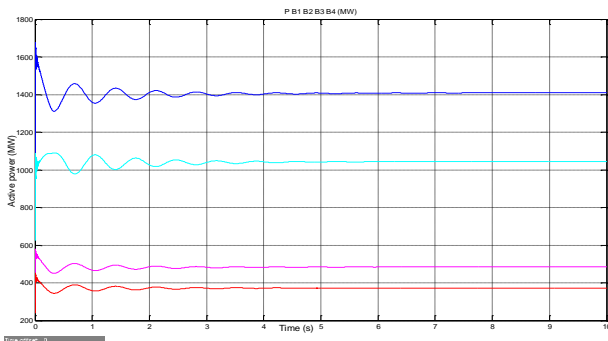


Fig. 3.5. X-axis Show time in sec. and Y-axis Show Active Power in Kw measured at all buses During Normal condition (No fault). The Transient Die out in Settling Time (4T).

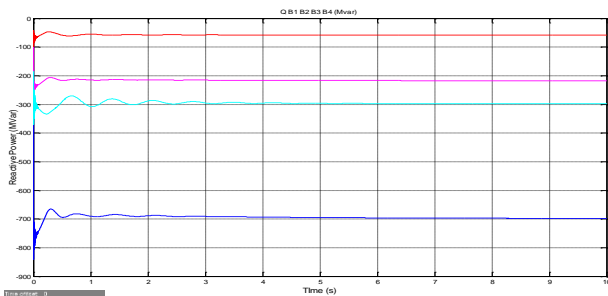


Fig. 3.6. X-axis Show time in sec. and Y-axis Show Reactive Power in Mvar at all buses During Normal condition (No fault). The Transient Die out in 2T.

3.2.2 CASE 2: SSSC under a three phase fault when POD is OFF

In this condition POD is kept 'off'. Under this condition the effect on power flow at bus no. 2 is shown in fig. 3.7. The fault clears at 0.5 sec as shown in fig. 3.7. In case 2 initially V_{qref} is set to zero. At 2 sec. it is set to $-0.08pu$ which makes SSSC to operate in inductive mode. At 6 sec. V_{qref} is set to $0.08 pu$ which operates SSSC in capacitive mode. A three phase fault is applied at Bus no. 4 at 0.33 sec. which lasts for 10 cycles. Figure 3.7 shows the power oscillations observed at bus no.2. The inductive and capacitive mode of operation can be observed easily. Fig 3.8 shows that how the injected voltage V_{qinj} follow the reference voltage V_{qref} .

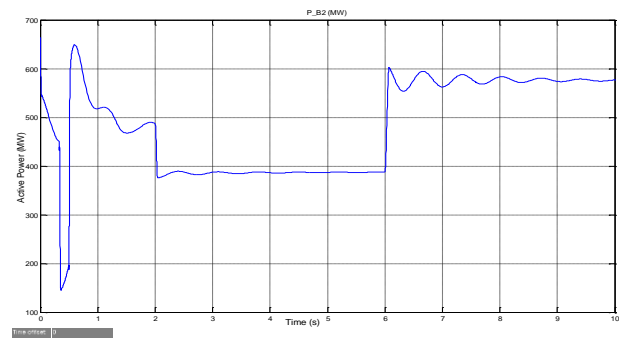


Fig. 3.7. X-axis Show time in sec. and Y-axis Show Active Power in Kw at bus no. 2 During Abormal condition ie fault. The Transient Die out in 8T (Almost double to normal case).

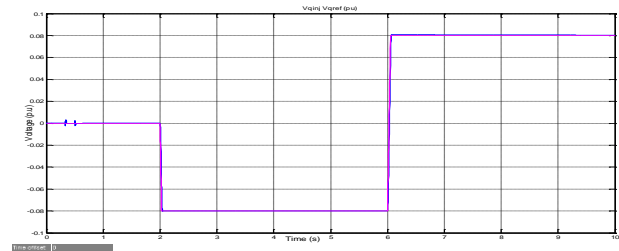


Fig. 3.8. X-axis Show time in sec. and Y-axis Show that how the injected voltage V_{qinj} follow the reference voltage V_{qref} .

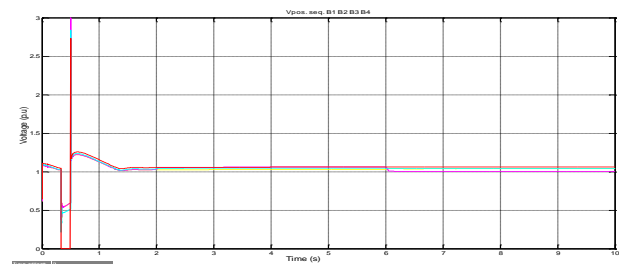


Fig. 3.9. X-axis Show time in sec. and Y-axis Show Positive sequence voltage at all buses During Abormal condition ie fault. The Transient Die out in 1.5 T.

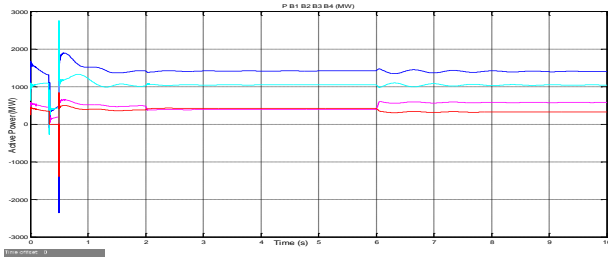


Fig. 3.10. X-axis Show time in sec. and Y-axis Show Active Power in Kw measured at all buses During Abormal condition ie fault. The Transient Die out in 2T.

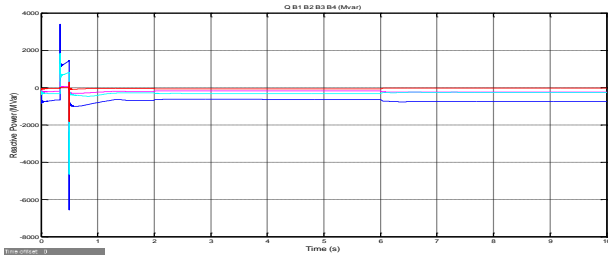


Fig. 3.11. X-axis Show time in sec. and Y-axis Show Reactive Power in Mvar Measured at all buses During Abormal condition ie fault.

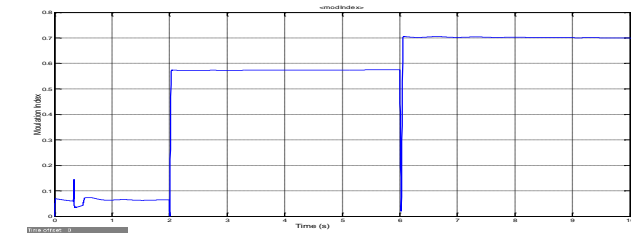


Fig. 3.12. X-axis Show time in sec. and Y-axis Show Modulation index During Abormal condition ie fault.

3.2.3 CASE 3: Test system with SSSC under a three phase fault and POD is ON :-

In this case, test system is kept under a symmetrical fault at 0.33 sec. and POD is kept on. The dynamic response of SSSC under this condition is shown below. As compare to fig.3.7 the power oscillations are removed very effectively. The output results illustrate that the power system oscillations are damped out very rapidly with the help of SSSC based damping controllers in few seconds.

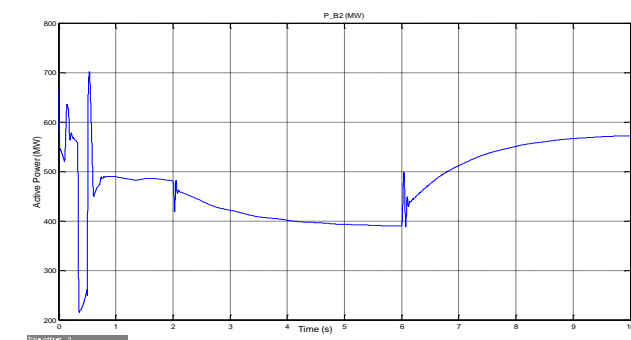


Fig. 3.13. X-axis Show time in sec. and Y-axis Show Active Power in Kw measured at buses no.2 During Abormal condition ie fault and POD is ON. As compare to fig.3.7 the power oscillations are removed very effectively. The output results illustrate that the power system oscillations are damped out very rapidly with the help of SSSC based damping controllers in few seconds.

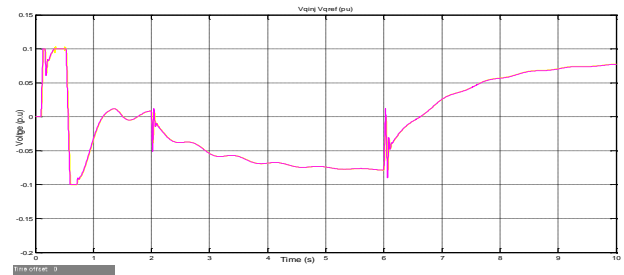


Fig. 3.14. X-axis Show time in sec. and Y-axis Show SSSC dynamic response for Voltage at three phase fault During Abormal condition ie fault and POD is ON. As compare to fig.3.8 the power oscillations are removed very effectively. The output results illustrate that the power system oscillations are damped out very rapidly with the help of SSSC based damping controllers in few seconds.

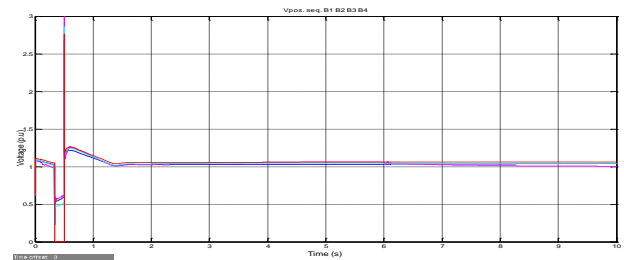


Fig. 3.15. X-axis Show time in sec. and Y-axis Show Positive Sequence Voltage at all buses During Abormal condition ie fault and POD is ON. As compare to fig.3.9 the power oscillations are removed very effectively. The output results illustrate that the power system oscillations are damped out very rapidly with the help of SSSC based damping controllers in few seconds.

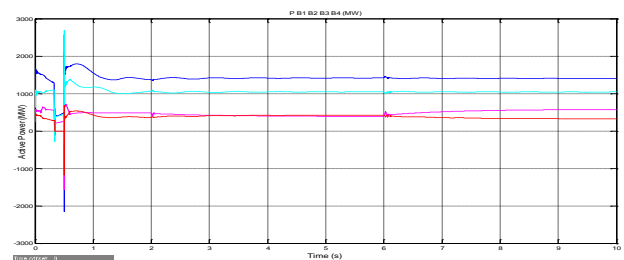


Fig. 3.16. X-axis Show time in sec. and Y-axis Show Active power measured at all buses in kw at all buses During Abormal condition ie fault and POD is ON. As compare to fig.3.10 the power oscillations are removed

very effectively. The output results illustrate that the power system oscillations are damped out very rapidly with the help of SSSC based damping controllers in few seconds.

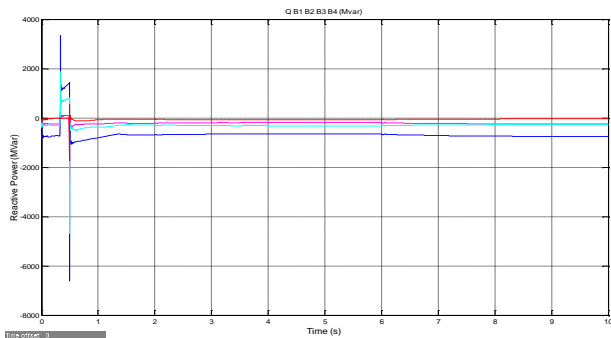


Fig. 3.17. X-axis Show time in sec. and Y-axis Show Reactive power in Mvar measured at all buses During Abormal condition ie fault and POD is ON. As compare to fig.3.11 the power oscillations are removed very effectively. The output results illustrate that the power system oscillations are damped out very rapidly with the help of SSSC based damping controllers in few seconds.

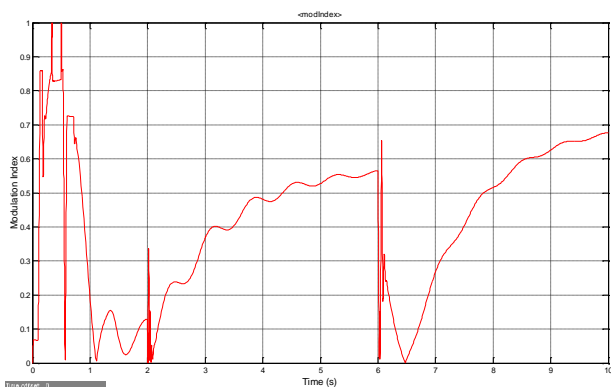


Fig. 3.18. X-axis Show time in sec. and Y-axis Show Modulation index During Abormal condition ie fault and POD is ON. As compare to fig.3.12 the power oscillations are removed very effectively. The output results illustrate that the power system oscillations are damped out very rapidly with the help of SSSC based damping controllers in few seconds.

It can be Seen From all of these figure that the POD Result is a Relatively Better System transient Response in term of the settling time.

IV. CONCLUSIONS

This thesis analyze the performance of a SSSC in a multi machine system in the presence of different faults is considered. The output results illustrate that the power system oscillations are damped out very rapidly with the help of SSSC based damping controllers in few seconds. The study reveals that SSSC is proficient to

enhance the power flow through the transmission line by injecting a fast changing voltage in series with the line. The injected voltage is in quadrature with line current and hence it can provide both inductive and capacitive compensation. PWM based and phase controller have both disadvantages and advantages, which makes the design process somewhat complicated. The dc voltage pre-set value in PWM-based controllers has to be carefully selected. As the modulation ratio lies between zero and one, the dc voltage should not be lower than the maximum of the requested SSSC output phase voltage in order to obtain proper control. On the other hand, if the dc side voltage is too high, the rating of both the GTO valves and dc capacitor has to be increased, which means higher installation costs. Not only that, a higher dc side voltage means a lower amplitude modulation ratio, and the lower modulation ratio results in higher harmonic distortion. Phase control allows the dc voltage to change according to the power system conditions, which is clearly advantageous, but it requires a more complicated controller and special and costly series transformers.

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