

Cooling Load Calculation during Summer & Duct Design and Duct Drafting for Commercial Project

S. M Azfar Hashmi^{#1}, Chanduri Rajendra Prasad^{*2}, Syed Faheem^{#3}, Syed Obaid Ur Rahman^{#4},
Syed Mujeeb Ali^{#5}

Mechanical Engineering Department of lords institute of engineering and technology, Jawaharlal Nehru Technological University, Hyderabad, Talengana, India

ABSTRACT

Human comfortness is essential now a day because of the improvement in life style and increasing central air conditioning is more reliable for easy operation with a lower maintenance cost. With large buildings such as commercial complex, auditorium, office buildings are provided with central air conditioning system. Educational and research institutions also need human comfortness, as the population of student community increase year by year. The effective designing of ducting in central air conditioning can provide human comfort, low power consumption, capital cost and improve aesthetic of building . This project establishes the results of duct designing for air conditioning using ASHRAE for a commercial building. Duct design items such as duct size, CFM each space pressure drop at each diffuser, elbow, T, taper reducer and duct class, duct material . Using ASHRAE and SMACNA fundamental hand book, maintaining ASHRAE and SMACNA standard.

Keywords : Overall heat transfer coefficient,HAP (Hourly analysis program),Duct designing,Duct drafting

I. INTRODUCTION

Heating, ventilation and air conditioning (HVAC) is the technology of indoor and vehicular environmental comfort. Its goal is to provide thermal comfort and acceptable indoor air quality. HVAC system design is a sub discipline of mechanical engineering, based on the principles of thermodynamics, fluid mechanics, and heat transfer. Refrigeration is sometimes added to the field's abbreviation as *HVAC&R* or *HVACR*, or ventilating is dropped as in *HACR*.

Energy efficiency can be improved more by installing central heating systems which allows more granular application of heat. Zones can be controlled by multiple thermostats. The HVAC industry is a worldwide enterprise, with roles including operation and maintenance, system design and construction, equipment manufacturing and sales, and in education and research. The HVAC industry was historically regulated by the manufacturers of HVAC equipment, but regulating and standards organizations such as *HARDI*, *ASHRAE*, *SMACNA*, *ACCA*, Uniform Mechanical Code, International Mechanical Code,

and *AMCA* have been established to support the industry and encourage high standards and achievement.

The starting point in carrying out an estimate both for cooling and heating depends on the exterior climate and interior specified conditions. However, before taking up the heat load calculation, it is necessary to find fresh air requirements for each area in detail, as pressurization is a building environment standards. It establishes the general principles of building environment design. It considers the need to provide a healthy indoor environment for the occupants as well as the need to protect the environment for future generations and promote collaboration among the various parties involved in building environmental design for sustainability. ISO16813 is applicable to new construction and the retrofit of existing buildings.

The building environmental design standard aims to:

- Provide the constraints concerning sustainability issues from the initial stage of the design process, with building and plant life cycle to be considered together with owning and operating costs from the beginning of the design process.

- Assess the proposed design with rational criteria for indoor air quality, thermal comfort, acoustical comfort, visual comfort, energy efficiency and HVAC system controls at every stage of the design process.

II. METHODS AND MATERIAL

A. Methodology

- Commercial building plan of 11634.5 square feet
- Calculation of floor, roof, wall and windows areas.
- Calculation of temperature difference (ΔT).
- Thermal resistance of wall, roof and windows.
- H.A.P 4.61.
- Overall heat transfer co – efficient.
- Ton of refrigerant.

B. Psychometric condition during summer in Hyderabad

Dry Bulb Temperature- 105°F

Relative Humidity-70-80%

As the above conditions for the citizens of Hyderabad is not comfortable. So, the air should be dehumidified and should bring the temperature at 72°F-76°F, and relative humidity to 50%-60%. For this cooling is required in a space.

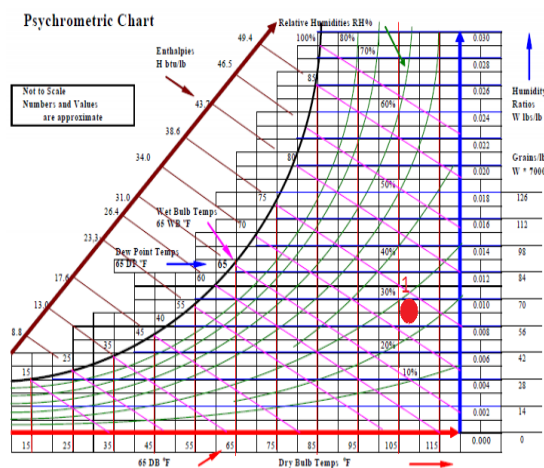


Figure 1: psychometric properties of air during summer

C. Design

For estimating cooling loads, one must consider the unsteady state processes, as the peak cooling load

occurs during the day time and the outside conditions also vary significantly throughout the day due to solar radiation. In addition, all internal sources add on to the cooling loads and neglecting them would lead to underestimation of the required cooling capacity and the possibility of not being able to maintain the required indoor conditions. Thus, cooling load calculations are inherently more complicated as it involves solving unsteady equations with unsteady boundary conditions and internal heat sources.

D. Cooling Load Calculation By Using HAP

(heat load calculation i.e. heat gain through all the sources)

- Application for summer
- Process is directly to cooling and dehumidification (required in wet summer)
- Cooling and humidification (required in dry summer like in desert areas where there is no water available for evaporation).

DEFINITION: The room cooling load is a rate at which the heat must be removed from the room air in order to maintain it at desired temperature and humidity.

E. Civil structure of building

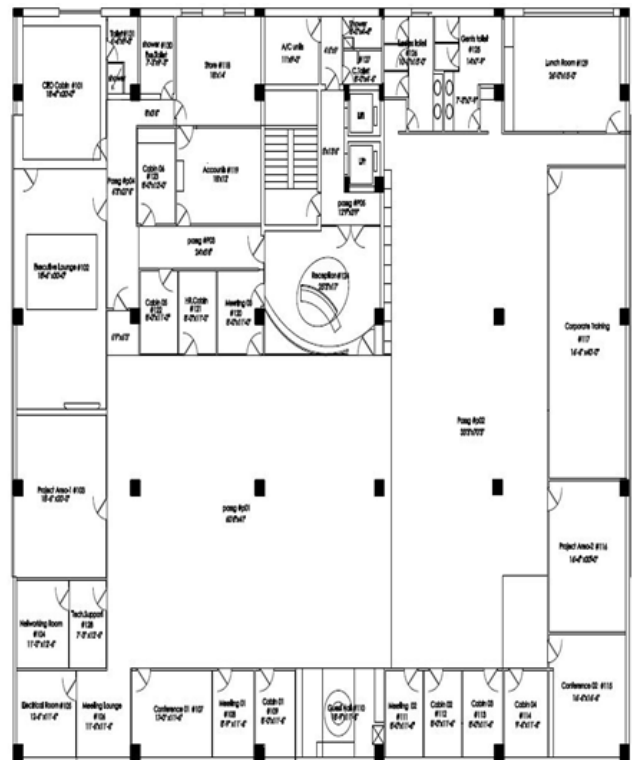


Figure 2: Civil structure of building

F. Gathering Data

The second step in the design process is to gather information necessary to model heat transfer processes in the building and to analyze operation of the HVAC equipment which heats and cools the building. This involves gathering data for the building, its environment and its HVAC equipment. Below, gathering of weather data, data for spaces in the building and data for the HVAC system will be discussed.

G. Gathering Weather Data

ASHRAE design weather conditions for Hyderabad will be used for this analysis. In addition to the ASHRAE data, we will use the period Mar through July as the design cooling months. This means cooling sizing calculations will only be performed for this range of months. We could use January through December as the calculation period. However, design weather conditions in Hyderabad are such that peak loads are most likely to occur during the summer or fall months. So we can reduce the set of calculation months to Mar through July to save calculation time without sacrificing reliability.

H. Gathering Space Data

1. Walls

One common wall construction is used for all exterior walls. The construction, consists of 8-inch lightweight concrete block. The exterior surface absorption is in the “dark” category. The overall U-value is 0.37 BTU/(hr-sqft-F). The overall weight is 87.3 lb/sqft.

2. Roofs

One uniform horizontal roof construction is used for this portion of the school building. The roof construction consists of half inch cement plaster, 4” Concrete block, half inch cement plaster. The exterior surface absorption is in the “dark” category. The overall U-value is 0.541 BTU/(hr-sqft-F). The overall weight is 43.6 lb/sqft. Note that in HAP the roof assembly must include all material layers from the exterior surface to the interior surface adjacent to the conditioned space.

3. Lighting

Recessed, unvented fluorescent lighting fixtures are used for all rooms in this portion of the school building. A lighting density of 1.00 W/sqft is used. For offices,

storage rooms and practice rooms we will use design day lighting levels of 100% from 0700 through 1700, the standard occupancy period for the offices, and 5% from 1800 through 2100 when lighting is reduced or operated intermittently for custodial work. This lighting profile applies for the days the building is in session. For weekends and holidays lighting levels of 0% are used.

4. Occupants

The maximum number of occupants varies by space and will be discussed later in this section. For all rooms “seated at rest” activity level will be used (230 BTU/hr/person sensible, 120 BTU/hr/person latent). For the music room the “office work” activity level will be used due to the higher level of activity in this room (245 BTU/hr/person sensible, 205 BTU/hr/person latent). For all rooms we will use design day occupancy levels of 100% for 0700 through 1700, the normal hours of operation for the building. Occupancy during the period 1800 through 2100 is very infrequent and will be ignored. Thus, occupancy levels of 0% will be used for all other hours of the day. This occupancy profile applies for days the school is in session. For weekends and holidays 0% occupancy is used for all hours.

5. SPACE DIMENSIONS

Table 1. Space Dimensions

SNO	ROOM NAME	R.NO	DIMENSIONS	AREA		PERIMETER		VOLUME		POSITIONAL	OCCUPANCY
				FLOOR	WALL	WALL	WALL	WALL	WALL		
1	CEG CHAMBER	101	15.5*15.0*2	232	372	368	74	103	355	120	5
2	EMERGENCY ROOM	102	15.5*15.0*2	232	372	368	74	103	355	120	5
3	PHYSICIAN OFFICE	103	15.5*15.0*2	232	372	368	74	103	355	120	5
4	PHYSICIAN ROOM	104	15.5*15.0*2	232	372	368	74	103	355	120	5
5	EMERGENCY ROOM	105	15.5*15.0*2	232	372	368	74	103	355	120	5
6	EMERGENCY ROOM	106	15.5*15.0*2	232	372	368	74	103	355	120	5
7	EMERGENCY ROOM	107	15.5*15.0*2	232	372	368	74	103	355	120	5
8	EMERGENCY ROOM	108	15.5*15.0*2	232	372	368	74	103	355	120	5
9	EMERGENCY ROOM	109	15.5*15.0*2	232	372	368	74	103	355	120	5
10	EMERGENCY ROOM	110	15.5*15.0*2	232	372	368	74	103	355	120	5
11	EMERGENCY ROOM	111	15.5*15.0*2	232	372	368	74	103	355	120	5
12	EMERGENCY ROOM	112	15.5*15.0*2	232	372	368	74	103	355	120	5
13	EMERGENCY ROOM	113	15.5*15.0*2	232	372	368	74	103	355	120	5
14	EMERGENCY ROOM	114	15.5*15.0*2	232	372	368	74	103	355	120	5
15	EMERGENCY ROOM	115	15.5*15.0*2	232	372	368	74	103	355	120	5
16	EMERGENCY ROOM	116	15.5*15.0*2	232	372	368	74	103	355	120	5
17	EMERGENCY ROOM	117	15.5*15.0*2	232	372	368	74	103	355	120	5
18	EMERGENCY ROOM	118	15.5*15.0*2	232	372	368	74	103	355	120	5
19	EMERGENCY ROOM	119	15.5*15.0*2	232	372	368	74	103	355	120	5
20	EMERGENCY ROOM	120	15.5*15.0*2	232	372	368	74	103	355	120	5
21	EMERGENCY ROOM	121	15.5*15.0*2	232	372	368	74	103	355	120	5
22	EMERGENCY ROOM	122	15.5*15.0*2	232	372	368	74	103	355	120	5
23	EMERGENCY ROOM	123	15.5*15.0*2	232	372	368	74	103	355	120	5
24	EMERGENCY ROOM	124	15.5*15.0*2	232	372	368	74	103	355	120	5
25	EMERGENCY ROOM	125	15.5*15.0*2	232	372	368	74	103	355	120	5
26	EMERGENCY ROOM	126	15.5*15.0*2	232	372	368	74	103	355	120	5
27	EMERGENCY ROOM	127	15.5*15.0*2	232	372	368	74	103	355	120	5
28	EMERGENCY ROOM	128	15.5*15.0*2	232	372	368	74	103	355	120	5
29	EMERGENCY ROOM	129	15.5*15.0*2	232	372	368	74	103	355	120	5
30	EMERGENCY ROOM	130	15.5*15.0*2	232	372	368	74	103	355	120	5
31	EMERGENCY ROOM	131	15.5*15.0*2	232	372	368	74	103	355	120	5
32	EMERGENCY ROOM	132	15.5*15.0*2	232	372	368	74	103	355	120	5
33	EMERGENCY ROOM	133	15.5*15.0*2	232	372	368	74	103	355	120	5
34	EMERGENCY ROOM	134	15.5*15.0*2	232	372	368	74	103	355	120	5
35	EMERGENCY ROOM	135	15.5*15.0*2	232	372	368	74	103	355	120	5

I. Gathering Air System Data

One air handling system will provide cooling and heating to the rooms in this wing of the commercial Building. Therefore, we will define one HAP air system to represent this equipment.

1. Equipment Type

A VAV rooftop unit will be used.

2. Ventilation

Outdoor ventilation airflow will be calculated using the ASHRAE Standard 62.1-2007 method. "Constant" control for ventilation will be used so the system uses the design flow of outdoor air at all times. Ventilation dampers are closed during the unoccupied period and the damper leak rate is 5%.

3. Cooling Coil

The system provides a constant 55 F supply air temperature to zone terminals. The DX cooling coil is permitted to operate in all months. The bypass factor for the cooling coil is 0.038 which is representative of the type of equipment we expect to select.

4. Preheat Coil

The rooftop unit contains a preheat coil to maintain minimum supply duct temperatures during the winter. The preheat coil is located downstream of the point where return air and outdoor ventilation air mix. The preheat set point is 52 F. The gas-fired heat exchanger in the rooftop unit is used for this purpose. The coil is permitted to operate in all months.

5. Supply Fan

The supply fan in the rooftop unit will be forward curved with variable frequency drive. The total static pressure for the system is estimated to be 3 in wg. The overall fan efficiency is 48%. The coil configuration is draw-thru.

6. Zoning

A zone is a region of the building with one thermostatic control. One zone will be created for each classroom.

The music room and its adjacent office, storage room and practice room will all be part of a single zone. Each corridor will also be zone. Therefore, a total of 9 zones will be created: one each for the six classrooms, one for the music room and two for the corridors.

7. Thermostats

Thermostat settings of 75 F occupied cooling, 80 F unoccupied cooling, 70 F occupied heating and 65 F unoccupied heating will be used in all zones. The throttling range will be 1.5 F. The schedule for fan and thermostat operation for the design day will designate 0700 through 2100 as "occupied" hours. This covers both the 0700-1700 operating hours for the school and the 1800-2100 period when custodial staff is present. All other hours will be "unoccupied". This profile applies for the school year which runs from August through June. During the shutdown month of July all hours will be designated as "unoccupied".

8. Supply Terminals

All zones use parallel fan powered mixing box terminals with 0.5 in wg total fan static, 50% overall fan efficiency and a 95 F heating supply temperature. Minimum supply airflow for the terminals is based on ASHRAE Standard 62.1-2007 requirements. We will specify minimum zone airflow as zero so the program will automatically use the Standard 62.1-2007 requirement to set the minimum damper position. The heat source for the reheat coils is electric resistance.

9. Sizing Criteria

Required zone airflow rates will be based on the peak sensible load in each zone. Required space airflow rates will be based on peak space loads for the individual spaces. Safety factors will be specified as zero. A margin of safety will be applied later during equipment selection.

After weather, space and HVAC system data has been gathered, it is entered into HAP. This is the third step in the design process. After entering the data into HAP the report will be generated by HAP itself.

III. RESULTS AND DISCUSSION

J. Report

Table 2. Air system sizing summary for AHU-001

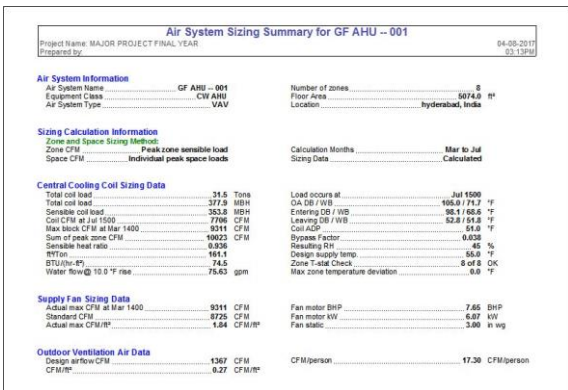


Table 3. Zone sizing summary for AHU-001

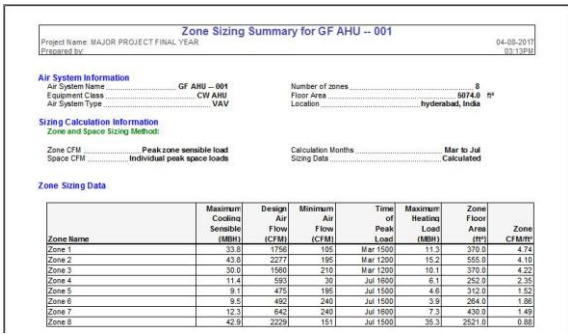


Table 4. Space load and Airflow for AHU-001

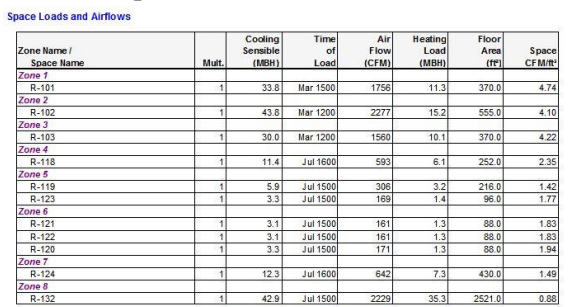


Table 5. Air system sizing summary for AHU-002

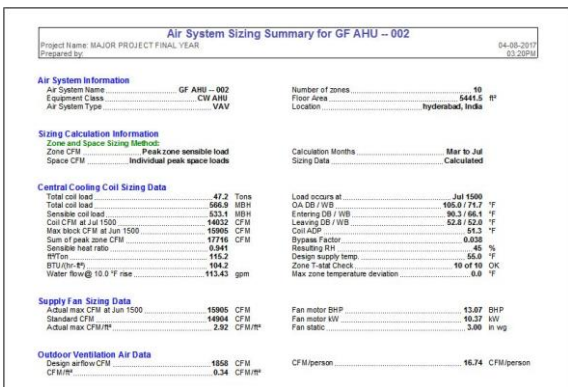


Table 6. Zone sizing summary for AHU-002

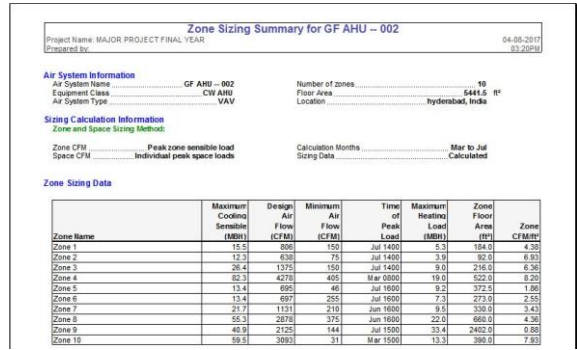


Table 7. Space load and Airflow for AHU-002

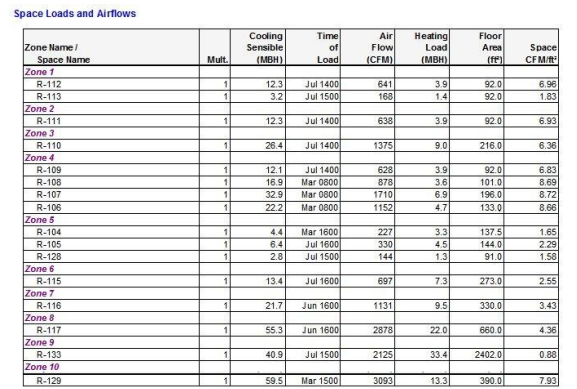
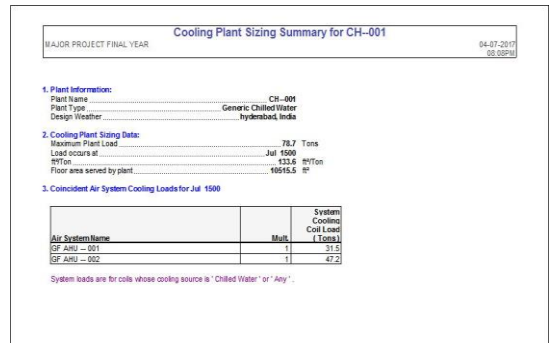


Table 8. cooling plant sizing summary for CH-001



K. Duct Designing & Terminal Selection of AHU001

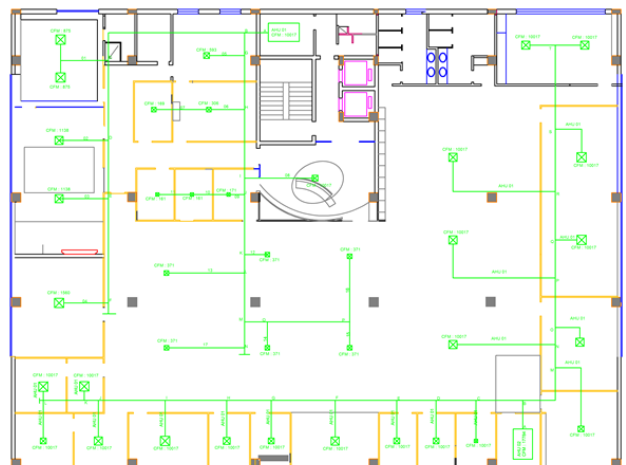


Figure 2. Single line drawing of AHU-001 & AHU-002
1. Main duct designing of AHU-001

Application: Commercial

Height of Main Duct: 18'' & 16'' (as per clearance above false ceiling).

Velocity: 2500 – 4000 FPM ~3000 FPM.

For section A to B

$$Q = 10017 \text{ CFM}$$

$$V = 3000 \text{ FPM}$$

From the friction chart in ASHRAE Hand Book we get $F = 0.445'' \text{ Wg}/100'$

Round duct size 25''

Rectangular duct size from equivalent rectangular duct dimension table 40'' X 14''.

For section B to C

$$Q = 5585 \text{ CFM}$$

$$V = 2600 \text{ FPM}$$

From the friction chart in ASHRAE Hand Book we get $F = 0.441'' \text{ Wg}/100'$

Total friction for duct B to C

$$F_p = (F/100) \times \text{length of duct}$$

$$F_p = (0.441''/100) \times 34' = 0.149'' \text{ Wg}$$

$$P_s = 0.9 \times \{(3000/4000)^2 - (2600/4000)^2\} = 0.126'' \text{ Wg}$$

P_s is less than F_p so it is not accepted, now chose more less velocity to increase static pressure.

$$Q = 5585 \text{ CFM}$$

$$V = 2400 \text{ FPM}$$

From the friction chart in ASHRAE Hand Book we get $F = 0.359'' \text{ Wg}/100'$

Total friction for duct B to C

$$F_p = (0.359''/100) \times 34' = 0.122'' \text{ Wg}$$

$$P_s = 0.9 \times \{(3000/4000)^2 - (2400/4000)^2\} = 0.182'' \text{ Wg}$$

Now p_s is greater than F_p , it is accepted so from the friction chart in ASHRAE Hand Book we get the duct dia 21''

From equivalent rectangular duct dimension table we get duct size 26'' X 14''.

Similarly proceeding further in tabular form below.

Table 9. Main duct designing of AHU-001

Sections	CFM	Velocity (FPM)	Friction (Wg/100')	Length of Duct (ft)	Friction parameter (Wg)	Static Pressure (Wg)	Equivalent Duct Dia (Inches)	Rect Duct Size (Inches)	Selected or Not
A to B	10017	3000	0.445	6	0.026	NA	24.7	14X20	*
B to C	5585	2600	0.441	34	0.149	0.126	19.2	14X20	X
B to D	5585	2600	0.359	34	0.122	0.182	20.7	14X20	*
C to D	2600	2000	0.362	17.25	0.062	0.03	17.9	14X19	X
D to E	2600	2000	0.254	17.25	0.043	0.29	16.4	14X22	*
E to F	2600	1800	0.27	12.5	0.033	0.042	16.6	14X19	*
F to G	1500	1800	0.26	22.5	0.058	0.03	14.4	14X11	X
G to H	1500	1800	0.2	22.5	0.045	0.072	14.3	14X12	*
H to I	4452	2000	0.423	5	0.021	0.06	17	14X18	*
I to J	3839	2000	0.554	11.5	0.063	0.062	16.5	14X19	X
J to K	3839	2000	0.452	11.5	0.025	0.117	17.1	14X18	*
K to L	3944	2000	0.362	14.75	0.057	0.064	16.7	14X19	*
L to M	3944	2000	0.308	14.75	0.045	0.099	16.4	14X18	*
M to N	2712	1800	0.268	9.5	0.0503	0.065	16.4	14X18	*
N to O	2229	1800	0.225	13	0.029	0.03	16	14X16	*
O to P	1858	1800	0.18	4.5	0.0081	0.03	14.4	14X14	*
Q to R	1478	1800	0.16	19.75	0.031	0.02	14	14X12	*
M to N	371	800	0.058	5.5	0.0021	0.018	8.2	14X8	*
M to O	1407	1800	0.246	9	0.0093	0.027	14.2	14X12	*
O to P	742	800	0.038	17.75	0.0138	0.018	13	14X10	*
Total Static Pressure					0.217				

2. Terminal Branch Designing

Branch 1

$$Q = 1749 \text{ CFM}$$

$$H = 14'' - 2'' = 12'' \text{ (height)}$$

$$F = 0.06'' \text{ Wg}/100'$$

From the friction chart in ASHRAE Hand Book we get $V = 900 \text{ FPM}$

Duct Dia = 19'' & Duct size = 28'' X 10''.

Similarly proceeding further in tabular form below.

Table 10. Branch duct designing

S.NO	CFM	HEIGHT	FRICITION (wg/100')	VELOCITY (FPM)	DUCT DIA	DUCT SIZE
1	1749	12"	0.06"	900	19"	26" X 12"
2	1138	10"	0.06"	800	16"	24" X 10"
3	1138	10"	0.06"	800	16"	24" X 10"
4	1560	12"	0.2"	1400	14"	14" X 12"
5	593	10"	0.06"	700	13"	14" X 10"
6	475	10"	0.06"	600	12"	12" X 10"
7	169	6"	0.06"	500	8"	10" X 6"
8	642	10"	0.06"	700	13"	14" X 10"
9	493	10"	0.06"	700	12"	12" X 10"
10	322	10"	0.06"	600	10"	10" X 10"
11	161	6"	0.06"	500	8"	10" X 6"
12	371	10"	0.06"	600	12"	10" X 10"
13	371	10"	0.06"	600	12"	10" X 10"
14	371	10"	0.06"	600	12"	10" X 10"
15	371	10"	0.06"	600	12"	10" X 10"
16	371	10"	0.06"	600	12"	10" X 10"
17	371	10"	0.06"	600	12"	10" X 10"

3. Diffuser Selection

Diffuser 1

$$Q = 875 \text{ CFM}$$

$V = 450 \text{ FPM}$ (velocity should be taken as branch velocity)

From the duct sizer we get

Neck Size = 12'' X 12''

Face Size = 15'' X 15'' (as per manufacturer).

Diffuser 2

$$Q = 875 \text{ CFM}$$

$V = 450 \text{ FPM}$ (velocity should be taken as branch velocity)

From the duct sizer we get

Neck Size = 12'' X 12''

Face Size = 15'' X 15''.

Similarly proceeding further in tabular form below.

Table 11. Diffuser Selection

DIFFUSER SELECTION BY DUCT SIZER				
S.NO	CFM	VELOCITY (FPM)	NECK SIZE	FACE SIZE
1	875	450	12"X 12"	15"X 15"
2	875	450	12"X 12"	15"X 15"
3	1138	800	15"X 15"	18"X 18"
4	1138	800	15" X 15"	18"X 18"
5	1560	900	18"X 18"	21"X 21"
6	593	700	12"X 12"	15"X 15"
7	306	600	9"X 9"	12"X 12"
8	169	500	9"X 9"	12"X 12"
9	642	700	12"X 12"	15"X 15"
10	171	650	6"X 6"	9"X 9"
11	161	600	6"X 6"	9"X 9"
12	161	500	6"X 6"	9"X 9"
13	371	600	9"X 9"	12"X 12"
14	371	600	9"X 9"	12"X 12"
15	371	600	9"X 9"	12"X 12"
16	371	600	9"X 9"	12"X 12"
17	371	600	9"X 9"	12"X 12"
18	371	600	9"X 9"	12"X 12"

L. Duct Designing & Terminal Selection of AHU002

1. Main duct designing of AHU-002

Application : Commercial

Height of Main Duct : 18'' & 16'' (as per clearance above false ceiling).

Velocity : 2500 – 4000 FPM ~3000 FPM.

Table 12. Main duct designing of AHU-001

[AHU 01] MAIN DUCT DESIGNING BY STATIC REGAIN METHOD									
Sections	CFM	Velocity (FPM)	Friction (wg/100')	Length of Duct (ft)	Friction pressure (Wg)	Static Pressure (Wg)	Equivalent Duct Dia (Inches)	Rect Duct Size (Inches)	Selected or Not
A to B	17784	3000	0.238	4	0.952	164	23	3824	*
B to C	7661	2000	0.432	8.5	0.366	0.603	23	3824	*
C to D	7693	2000	0.362	8.5	0.318	0.602	23	3824	*
D to E	7652	2000	0.312	8.5	0.268	0.596	23	3824	*
E to F	8424	2200	0.265	15.25	0.403	0.651	23	3824	*
F to G	3089	2000	0.243	13.75	0.333	0.647	22	3822	*
G to H	4411	1800	0.2	9.5	0.19	0.64	21	3822	*
H to I	3533	1800	0.17	13.25	0.222	0.638	20	3820	*
I to J	3822	1400	0.182	14.25	0.262	0.633	18	3812	*
J to K	871	1200	0.229	3	0.686	0.629	18	3816	*
K to L	557	1000	0.362	8.75	0.314	0.627	18	3816	*
L to M	9923	2000	0.375	3	0.1125	0.663	26	3832	*
M to N	9226	2000	0.325	6.75	0.218	0.662	25	3832	*
N to O	8528	2400	0.278	5.75	0.155	0.656	25	3832	*
O to P	7887	2200	0.243	12.25	0.292	0.651	25	3830	*
P to Q	6679	2000	0.269	9.75	0.269	0.647	25	3830	*
Q to R	3240	1800	0.18	9.75	0.177	0.64	23	3828	*
R to S	4522	1800	0.146	3	0.438	0.638	23	3824	*
S to T	3093	1400	0.132	24.25	0.312	0.633	20	3820	*
TOTAL STATIC PRESSURE						1.394			

2. Terminal Branch Designing

Table 13. Branch duct designing

BRANCH DUCT DESIGNING WITH EQUAL FRICTION METHOD						
S.NO	CFM	HEIGHT	FRICTION (wg/100')	VELOCITY (FPM)	DUCT DIA	DUCT SIZE
1	168	6"	0.06"	500	8"	10"X 6"
2	641	10"	0.06"	700	13"	14"X 10"
3	638	10"	0.06"	700	13"	14"X 10"
4	1375	14"	0.06"	900	18"	18"X 14"
5	628	10"	0.06"	700	13"	14"X 10"
6	878	14"	0.06"	800	15"	16"X 14"
7	1710	14"	0.06"	900	19"	20"X 14"
8	1152	14"	0.06"	800	16"	16"X 14"
9	330	8"	0.06"	600	10"	10"X 8"
10	227	8"	0.06"	500	9"	10"X 18"
11	114	6"	0.06"	500	7"	10"X 6"
12	697	10"	0.06"	700	14"	10"X 16"
13	1131	14"	0.06"	800	16"	16"X 14"
14	708	10"	0.06"	700	14"	16"X 10"
15	1439	14"	0.06"	800	18"	20"X 14"
16	708	10"	0.06"	700	14"	16"X 10"
17	1439	14"	0.06"	800	18"	20"X 14"
18	708	10"	0.06"	700	14"	16"X 10"
19	1546	10"	0.06"	900	18"	20"X 10"
20	1546	10"	0.06"	900	18"	20"X 10"

3. Diffuser Selection

Table 14. Diffuser Selection

DIFFUSER SELECTION BY DUCT SIZER				
S.NO	CFM	VELOCITY (FPM)	NECK SIZE	FACE SIZE
1	168	500	9"X 9"	12"X 12"
2	641	700	12"X 12"	15"X 15"
3	638	700	12"X 12"	15" X 15"
4	1375	900	18"X 18"	21"X 21"
5	628	700	12"X 12"	15" X 15"
6	878	800	15" X 15"	18"X 18"
7	1710	900	18" X 18"	21"X 21"
8	1152	800	15" X 15"	18"X 18"
9	330	600	9"X 9"	12"X 12"
10	227	500	9"X 9"	12"X 12"
11	114	500	6"X 6"	9"X 9"
12	697	700	12"X 12"	15" X 15"
13	1131	800	15" X 15"	18"X 18"
14	708	700	12"X 12"	15" X 15"
15	1439	800	18"X 18"	21"X 21"
16	708	700	12"X 12"	15" X 15"
17	1439	800	18"X 18"	21"X 21"
18	708	700	12"X 12"	15" X 15"
19	1546	800	18"X 18"	21"X 21"
20	1546	800	18"X 18"	21"X 21"

Table 15. total cooling load of the building

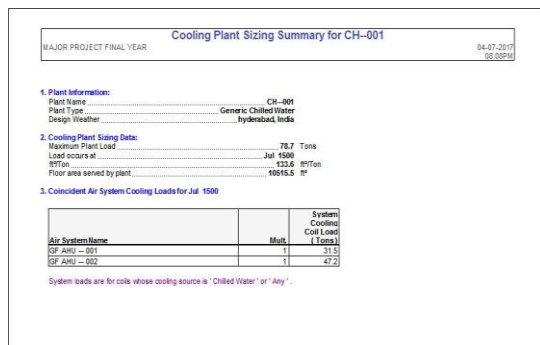
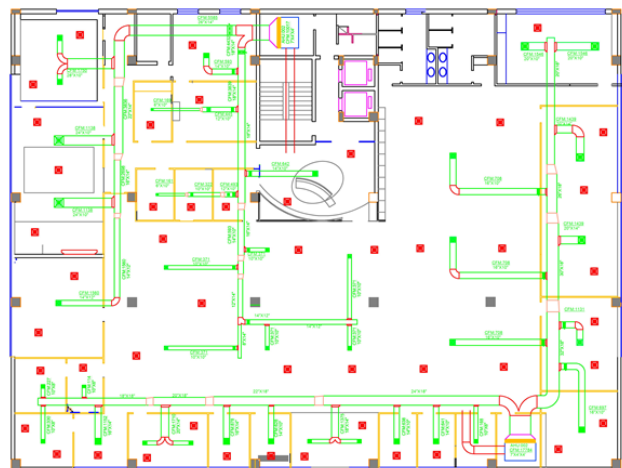


Figure 3. Double line drawing of AHU-001 & AHU-002



IV. CONCLUSION

This project briefly explains how to perform cooling load calculation in H.A.P 4.61 for humidifying the air and bring the psychometric properties at a comfort zone for human body in summer season.

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